

HC.1 FE Weak Statement Algorithm Steps

The (heat conduction) problem statement

$$L(T) = 0 \text{ on } \Omega + \text{BCs}$$

Approximate solution, with associated error

$$T^N(x) = \sum_{\alpha=1}^N \Psi_{\alpha}(x) Q_{\alpha}$$

$$T(x) = T^N(x) + e^N(x)$$

Minimize the error via Galerkin weak statement

$$\text{GWS}^N \equiv \int_{\Omega} \Psi_{\beta}(x) L(T^N) dx \equiv 0, \quad 1 \leq \beta \leq N$$

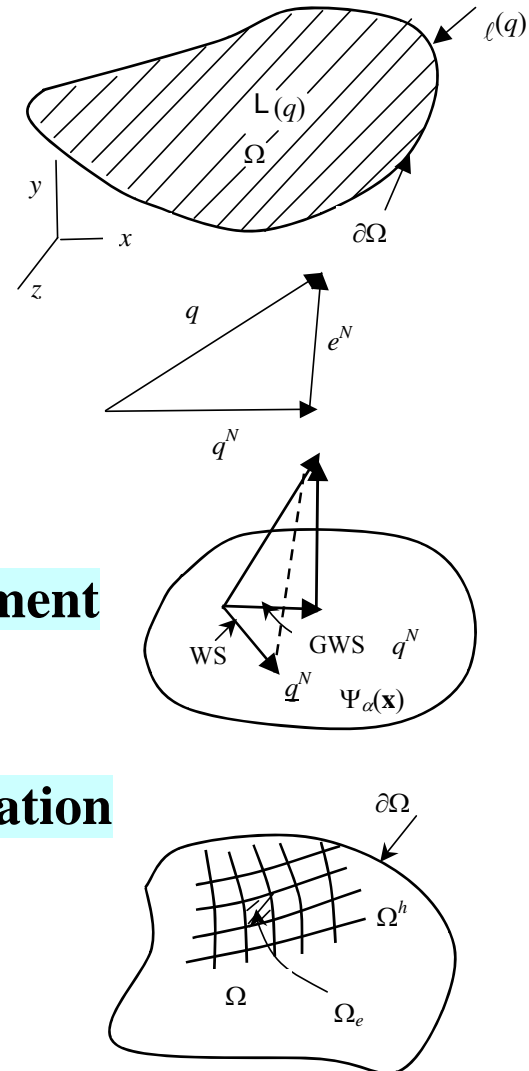
Implement GWS^N via FE discrete approximation

$$\Omega \Rightarrow \Omega^h \equiv \cup_e \Omega_e$$

$$T^N \equiv T^h(x) \Rightarrow \cup_e T_e(x), \quad \text{GWS}^N \Rightarrow \text{GWS}^h$$

Solve matrix statement

$$\text{GWS}^h \Rightarrow [\text{Matrix}]\{Q\} = \{b\}, \text{ hence evaluate error } e^h(x)$$



HC.2 An Example, Heat Conduction in a Slab

Example problem

$$\mathcal{L}(T) = -\frac{d}{dx}\left(k\frac{dT}{dx}\right) - s = 0, \quad \text{on } 0 < x < L$$

$$\ell(T) = -k\frac{dT}{dx} - f = 0 \quad \text{at } x = 0$$

$$T(L) = T_b \quad \text{at } x = L$$

Analytical solution

$$T(x) = \frac{sL^2}{2k}\left[1 - \left(\frac{x}{L}\right)^2\right] + \frac{fL}{k}\left(1 - \frac{x}{L}\right) + T_b$$

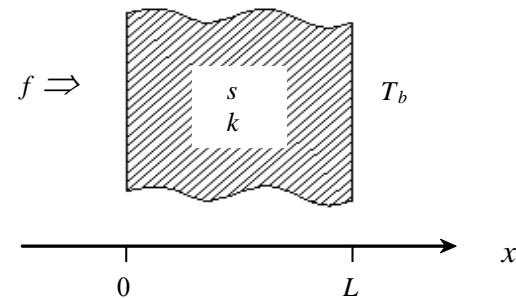
Any approximate solution

$$T^N(x) = \sum_{\alpha=1}^N \Psi_{\alpha}(x) Q_{\alpha} = Q_1 \Psi_1(x) + Q_2 \Psi_2(x) + \dots + Q_N \Psi_N(x)$$

For this simple problem, $T^N \Rightarrow T(x)$ for $N = 3$ via

$$Q_1 = \frac{sL^2}{2k}, Q_2 = \frac{fL}{k}, Q_3 = T_b; \Psi_1 = 1 - \left(\frac{x}{L}\right)^2, \Psi_2 = 1 - \left(\frac{x}{L}\right), \Psi_3 = 1$$

problem data



HC.3 Approximation, Constraint on Error

Any approximation

$$T^N(x) = \sum_{\alpha=1}^N \Psi_{\alpha}(x) Q_{\alpha}$$

The error in T^N is e^N , recall

$$T(x) = T^N(x) + e^N(x)$$

No knowledge of e^N exists, however $\mathbf{L}(T^N) = -\mathbf{L}(e^N)$

$$\mathbf{L}(T^N) = -\frac{d}{dx} \left(k \frac{dT^N}{dx} \right) - s \neq 0$$

Error minimized via Galerkin weak statement

$$\text{GWS}^N \equiv \int \Psi_{\beta}(x) \mathbf{L}(T^N) dx \equiv 0, 1 \leq \beta \leq N$$

HC.4 Galerkin Weak Statement, Minimum Error

Approximation

$$T^N(x) \equiv \sum_{\alpha=1}^N \Psi_{\alpha}(x) Q_{\alpha}$$

Galerkin weak statement

$$\text{GWS}^N \equiv \int_{\Omega} \Psi_{\beta}(x) \left[-\frac{d}{dx} \left(k \frac{dT^N}{dx} \right) - s \right] dx \equiv 0, \quad \text{for } 1 \leq \beta \leq N$$

Integrating by parts, substituting $T^N(x)$ and BC f_n

$$\text{GWS}^N = \sum_{\alpha=1}^N \left(\int_{\Omega} \frac{d\Psi_{\beta}}{dx} k \frac{d\Psi_{\alpha}}{dx} dx \right) Q_{\alpha} - \int_{\Omega} \Psi_{\beta} s dx - k \frac{dT^N}{dx} \Psi_N \Big|_{x=L} - f_n \Psi_1 \Big|_{x=0} = 0$$

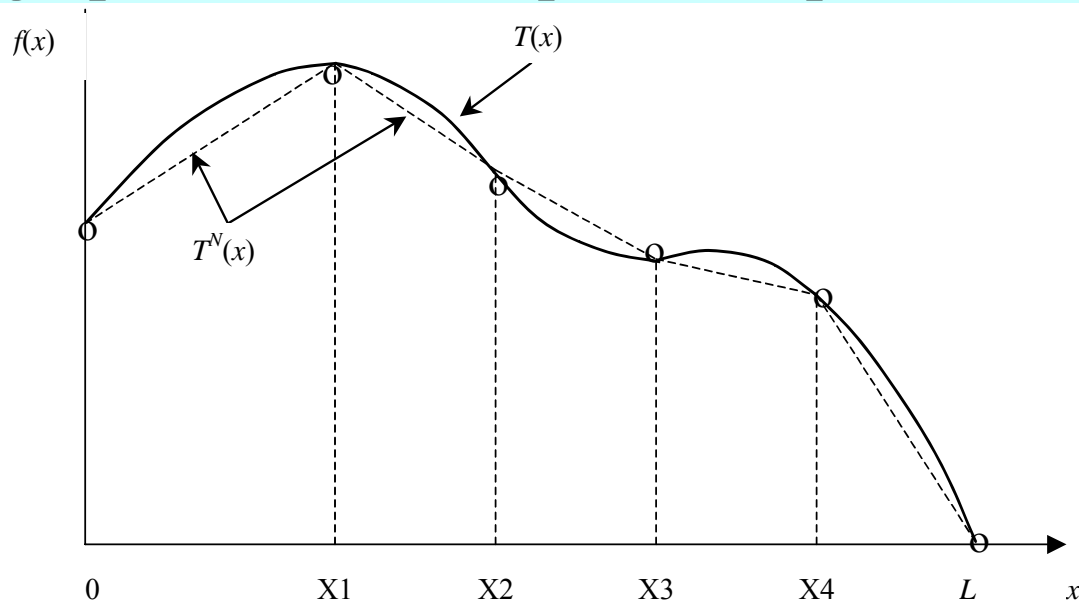
for $1 \leq \beta \leq N$, and heat flux BC is directly *embedded*

HC.5 Trial Functions, Interpolation

To complete the integrals in the GWS^N

⇒ must specify the trial space $\Psi_\alpha(x)$, $1 \leq \alpha \leq N$

Lagrange piecewise interpolation provides insight



Interpolation *error* can be adjusted by adding knots “o”

⇒ *nodes* of the FE discretization of $\Omega \Rightarrow \Omega^h = \cup_e \Omega_e$

HC.6 Discrete Approximation, Finite Element Basis

For $N = 3$ node FE mesh

$$T^N(x) = \sum_{\alpha=1}^{N=3} \Psi_{\alpha}(x) Q_{\alpha}$$

$$= \Psi_1 Q_1 + \Psi_2 Q_2 + \Psi_3 Q_3$$

Global trial functions $\Psi_{\alpha}(x)$

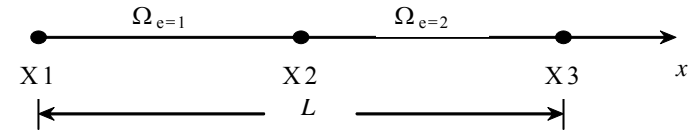
$$\Psi_{\alpha}(x \Rightarrow \text{node } (\alpha)) \equiv 1$$

$$\Psi_{\alpha}(x \Rightarrow \text{node } (\beta \neq \alpha)) \equiv 0$$

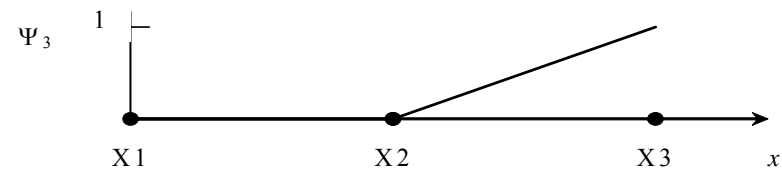
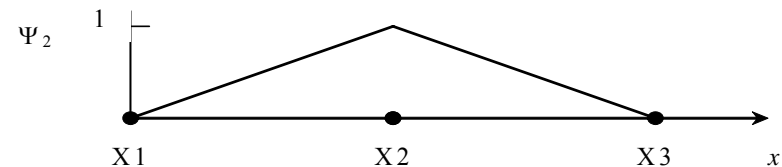
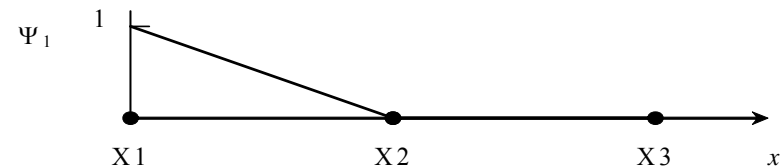
Local finite element basis $\{N\}$

$$\{N\} = \left\{ \begin{array}{l} n_1 = \frac{XR - x}{XR - XL} \\ n_2 = \frac{x - XL}{XR - XL} \end{array} \right\}_e$$

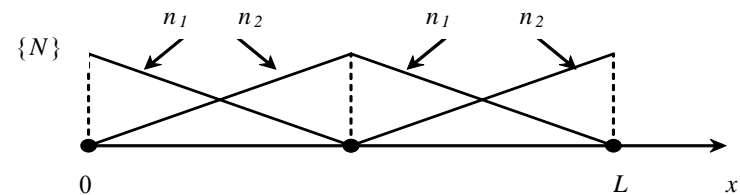
on every (!) element Ω_e



(a) 3-node discretization Ω^h of Ω



(b) trial function set Ψ_{α} , $1 \leq \alpha \leq 3$



(c) finite element basis

HC.7 Finite Element Matrix Library

GWS^N first term derivatives, subscripts \Rightarrow matrices

$$\int_{\Omega} \frac{d\psi_{\beta}}{dx} \frac{d\psi_{\alpha}}{dx} dx Q_{\alpha} \Rightarrow \int_{\Omega_e} \frac{d\{N\}}{dx} \frac{d\{N\}^T}{dx} dx \{Q\}_e, \quad \text{and} \quad \frac{dn_i}{dx} = \begin{cases} -1/l_e, i=1 \\ 1/l_e, i=2 \end{cases} = \frac{d\{N\}}{dx}$$

The integral of matrix products on Ω_e is

$$\begin{aligned} \int_{\Omega_e} \frac{d\{N\}}{dx} k \frac{d\{N\}^T}{dx} dx \{Q\}_e &= k \int_0^{l_e} \frac{1}{l_e} \begin{Bmatrix} -1 \\ 1 \end{Bmatrix} \frac{1}{l_e} \{-1 \quad 1\} dx \{Q\}_e \\ &= \frac{k}{l_e^2} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \int_0^{l_e} dx \{Q\}_e = \frac{k}{l_e} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \{Q\}_e \end{aligned}$$

For the constant source term

$$\int_{\Omega_e} \{N\} s dx = s \int_0^{l_e} \begin{Bmatrix} n_1 \\ n_2 \end{Bmatrix} dx = \frac{s l_e}{2} \begin{Bmatrix} 1 \\ 1 \end{Bmatrix}$$

Boundary conditions require no integration

HC.8 Finite Element Data Evaluations

The FE discrete implementation process yields

$$\text{GWS}^N \Rightarrow \text{GWS}^h = \sum_e \{\text{WS}\}_e$$

$$\{\text{WS}\}_e = \frac{k}{l_e} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \{Q\}_e - \frac{s l_e}{2} \begin{Bmatrix} 1 \\ 1 \end{Bmatrix} - k \frac{dT}{dx} \begin{Bmatrix} -\delta_{e1} \\ \delta_{eM} \end{Bmatrix}$$

δ_{ej} is a Kronecker delta on/off switch

Every contribution to $\{\text{WS}\}_e$ involves a product

$$\{\text{WS}\}_e = (\text{data})_e \times [\text{FE matrix}]$$

$$\begin{aligned} \text{for } e = 1: \quad \{\text{WS}\}_1 &= \frac{k}{l_1} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \{Q\}_{e=1} - \frac{s l_1}{2} \begin{Bmatrix} 1 \\ 1 \end{Bmatrix} - k \frac{dT}{dx} \begin{Bmatrix} -\delta_{11} \\ 0 \end{Bmatrix} \\ &= \frac{k}{L/2} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{Bmatrix} Q1 \\ Q2 \end{Bmatrix} - \frac{sL/2}{2} \begin{Bmatrix} 1 \\ 1 \end{Bmatrix} - \begin{Bmatrix} f \\ 0 \end{Bmatrix} \end{aligned}$$

$$\text{for } e = 2: \quad \{\text{WS}\}_2 = \frac{k}{L/2} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{Bmatrix} Q2 \\ Q3 \end{Bmatrix} - \frac{sL}{4} \begin{Bmatrix} 1 \\ 1 \end{Bmatrix} + \begin{Bmatrix} 0 \\ F3 \end{Bmatrix}$$

HC.9 FE Weak Statement Assembly over Ω^h

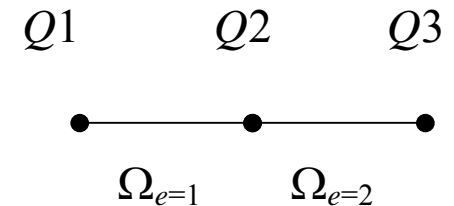
GWS^h is a matrix statement, i.e.,

$$\text{GWS}^h = \sum_e \{\text{WS}\}_e = [\text{Matrix}] \{Q\} - \{b\} = \{0\},$$

$$\{Q\} = \begin{Bmatrix} Q1 \\ Q2 \\ Q3 \end{Bmatrix}$$

[Matrix] and {b} involve a row summation process

$$[\text{Matrix}] = \sum_{e=1}^M [\text{Matrix}]_e$$



$$= \frac{2k}{L} \begin{bmatrix} 1 & -1 & 0 \\ -1 & 1 & 0 \\ 0 & 0 & 0 \end{bmatrix} + \frac{2k}{L} \begin{bmatrix} 0 & 0 & 0 \\ 0 & 1 & -1 \\ 0 & -1 & 1 \end{bmatrix} = \frac{2k}{L} \begin{bmatrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{bmatrix}$$

$$\{b\} = \sum_{e=1}^2 \{b\}_e = \frac{sL}{4} \begin{Bmatrix} 1 \\ 1 \\ 0 \end{Bmatrix} + \begin{Bmatrix} f_n \\ 0 \\ 0 \end{Bmatrix} + \frac{sL}{4} \begin{Bmatrix} 0 \\ 1 \\ 1 \end{Bmatrix} + \begin{Bmatrix} 0 \\ 0 \\ -F3 \end{Bmatrix}$$

assembly is universally valid for 1-D, 2-D and 3-D problems (!)

HC.10 Matrix Statement Solution, BCs

Assembling GWS^h over $M = 2$ FE domains Ω_e yields

$$\begin{bmatrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{bmatrix} \begin{Bmatrix} Q_1 \\ Q_2 \\ Q_3 \end{Bmatrix} = \frac{sL^2}{8k} \begin{Bmatrix} 1 \\ 2 \\ 1 \end{Bmatrix} + \frac{L}{2k} \begin{Bmatrix} f \\ 0 \\ -F_3 \end{Bmatrix}$$

Substitute BC $Q_3 = T_b$, move unknown flux F_3 to left

$$\begin{bmatrix} 1 & -1 & 0 \\ -1 & 2 & 0 \\ 0 & -1 & L/2k \end{bmatrix} \begin{Bmatrix} Q_1 \\ Q_2 \\ F_3 \end{Bmatrix} = \frac{sL^2}{8k} \begin{Bmatrix} 1 \\ 2 \\ 1 \end{Bmatrix} + \begin{Bmatrix} fL/2k \\ T_b \\ -T_b \end{Bmatrix}$$

As QM equations are *decoupled* from F_3 , Cramer's rule

$$\begin{Bmatrix} Q_1 \\ Q_2 \end{Bmatrix} = \begin{bmatrix} 1 & -1 \\ -1 & 2 \end{bmatrix}^{-1} \begin{Bmatrix} \frac{L}{2k} \left(\frac{sL}{4} + f_n \right) \\ \frac{sL^2}{4k} + T_b \end{Bmatrix} = \begin{Bmatrix} \frac{sL^2}{2k} + \frac{fL}{k} + T_b \\ \frac{3sL^2}{8k} + \frac{fL}{2k} + T_b \end{Bmatrix}$$

then solve for $F_3 = sL + f$

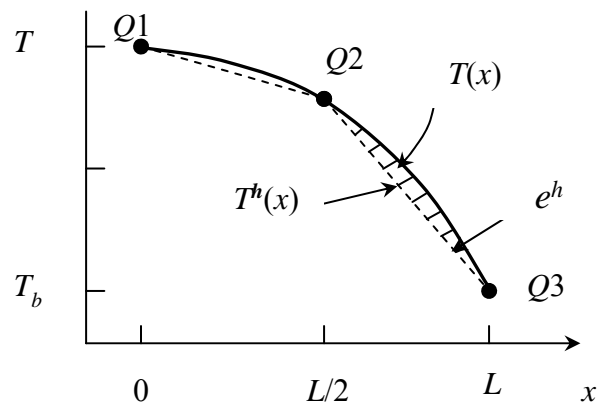
HC.11 Solution Accuracy, Error Distribution

The FE GWS^h nodal array $\{Q\}$ agrees with analytical solution

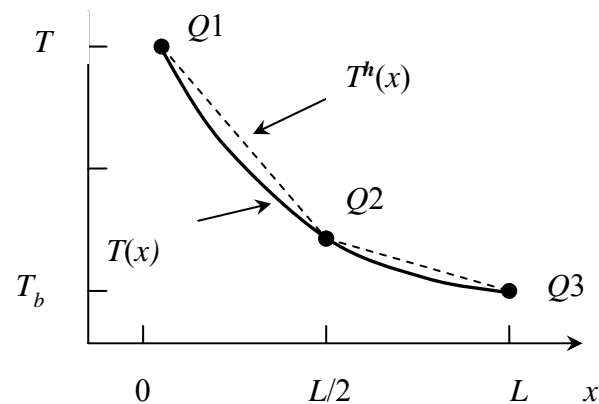
- this problem statement is very elementary
- concept of piecewise-continuous FE basis $\{N\}$ verified

T^h is still only an approximation!

- Taylor series *error* estimate: $e^h \approx O(\ell_e^2)$



(a) Positive source term s



(b) Negative source term s

HC.12 Boundary Heat Flux Computation

Boundary heat fluxes can be computed via

differentiating $T^h(x)$ at $x = L$

GWS h matrix solution for $F3$

Differentiating T^h at $x = L$ yields

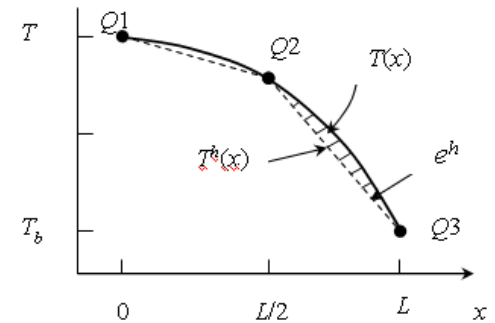
$$-k \frac{dT_{e=2}}{dx} = -\frac{k}{L/2} \left[T_b - \left(\frac{3sL^2}{8k} + \frac{f_n L}{2k} + T_b \right) \right] = \frac{3sL}{4} + f_n$$

\Rightarrow *inexact* (same as FD result)

Solving for $F3$ from GWS h matrix statement

$$F3 = -k \frac{dT^N}{dx} \Big|_{x=L} = -\frac{k}{L/2} \left[T_b - \left(T_b + \frac{f_n L}{2k} + \frac{3sL^2}{8k} \right) - \frac{sL^2}{8k} \right] = sL + f_n$$

\Rightarrow *exact!*



(a) Positive source terms

HC.13 Error Estimate, Quantization

Taylor series (TS) truncation error (TE) estimate

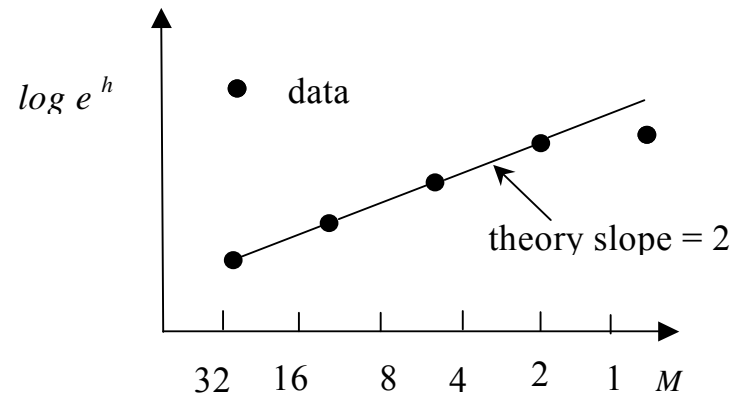
$$e^h \approx O(l_e^2) \equiv C l_e^2$$

Quantization of error uses uniform mesh refinement

meshes : $\Omega^h, \Omega^{h/2}, \Omega^{h/4}, \dots$
solutions : $T^h + e^h = T = T^{h/2} + e^{h/2} = \dots$
clear C: $e^h = 2^2 e^{h/2}$
hence : $T^{h/2} - T^h \equiv \Delta T^{h/2} = (2^2 - 1) e^{h/2} \Rightarrow e^{h/2} = \Delta T^{h/2}/3$

Assessment of theory validity

$$\begin{aligned} \text{slope} &\equiv \frac{\text{rise}}{\text{run}} \\ &= \frac{\log(e^{h/M}) - \log(e^{h/2M})}{\log(l_e) - \log(l_e/2)} \\ &= \log(e^{h/M} / e^{h/2M}) / \log 2 \end{aligned}$$



HC.14 Error Estimation, Energy Norm



Improved error estimate uses entire solution via a “norm”

$$\text{energy norm} \equiv \|T\|_E^h \equiv \frac{1}{2} \int_{\Omega} k \frac{dT^h}{dx} \frac{dT^h}{dx} d\tau \Rightarrow \frac{1}{2} \sum_e^M \{Q\}_e^T [\text{DIFF}]_e \{Q\}_e$$

Uniform mesh refinement study

$$\|T^h\|_E + \|e^h\|_E = \|T\|_E = \|T^{h/2}\|_E + \|e^{h/2}\|_E = \dots$$

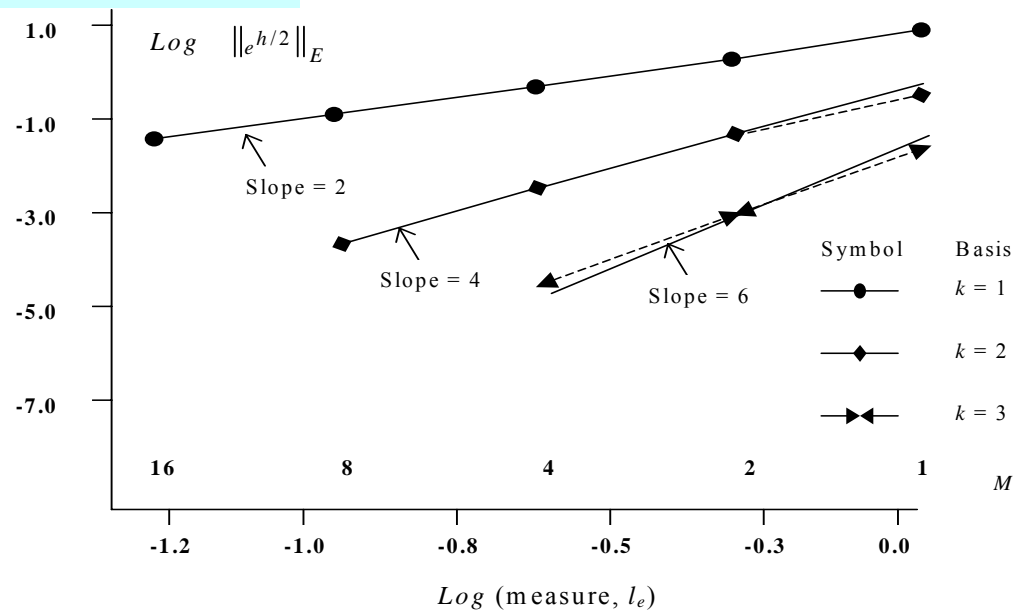
asymptotic convergence: $\|e^h\|_E \leq C_k \ell_e^{2k} \|\text{data}\|_{L2}^2$

error estimator

$$\|e^{h/2}\|_E = \frac{\Delta \|T^{h/2}\|_E}{2^{2k} - 1}$$

confirmation of theory

$$\text{slope} = \frac{\log \left[\frac{\|e^{h/M}\|_E}{\|e^{h/2M}\|_E} \right]}{\log 2}$$



HC.15 Error Quantization, $\{N_1\}$ FE Solution

Results from the computer lab exercise

Q_{max}

Mesh	M	l_e	$Q_1 \cdot 10^2$	$e^{h/2}$ (est.)	slope
Ω^h	1	1.00000	2.50000		
$\Omega^{h/2}$	2	0.50000	2.50000	0.000000	
$\Omega^{h/4}$	4	0.25000	2.50000	0.000000	
$\Omega^{h/8}$	8	0.12500	2.50000	0.000000	
$\Omega^{h/16}$	16	0.06250	2.50000	0.000000	
$\Omega^{h/32}$	32	0.03125	2.50000	0.000000	
$\Omega^{h/64}$	64	0.01563	2.50000	0.000000	

$\|e^h\|_E$

Mesh	M	l_e	$\ T^{h/2}\ _E 10^4$	$\ e^{h/2}\ _E$ (est)	slope
Ω^h	1	1.00000	1.12501		
$\Omega^{h/2}$	2	0.50000	1.15625	104.1667	
$\Omega^{h/4}$	4	0.25000	1.16406	26.04170	1.9999
$\Omega^{h/8}$	8	0.12500	1.16601	6.510417	2.0000
$\Omega^{h/16}$	16	0.06250	1.16650	1.627603	2.0000
$\Omega^{h/32}$	32	0.03125	1.16663	0.406902	1.9999
$\Omega^{h/64}$	64	0.01563	1.16663	0.101725	2.0000